

Willard M. Bleick

ORBITAL TRANSFER IN MINIMUM TIME

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Professor of Mathematics and Mechanics

RESEARCH PAPER NO. 34

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W. E. BLEICK,* U. S. Naval Postgraduate School

1. Introduction. The problem of orbital transfer discussed here is that of scheduling the direction p of constant momentum thrust of a rocket, which loses mass at a constant rate, so that it transfers to an earth satellite orbit, with known elements of time, position and velocity, in a minimum time T after launching of the rocket. The launching conditions are assumed to be fixed. This situation is illustrated in Figure 1 for the case of a circular orbit. The sector angle B at which the rocket enters orbit will be called the rendezvous angle. To aid the discussion imaginary physical rendezvous of the rocket and satellite is assumed to occur at this angle. The time of rocket launch to achieve actual physical rendezvous can be determined, of course, only after both of the unknowns T and B have been found. The problem is set up as a calculus of variations problem of the Lagrange type, and is solved by an iterative process in which an initial approximation to the angle B is estimated.

A non-rotating Oxy rectangular coordinate system with origin at the earth's center is used. The coordinates and velocity components of the rocket and target satellite are denoted by x, y, u, v and X, Y, U, V respectively. For simplicity the equations of motion of rocket and target will be written in a "non-dimensional" form by the use of suitable units. The unit of length is taken as the

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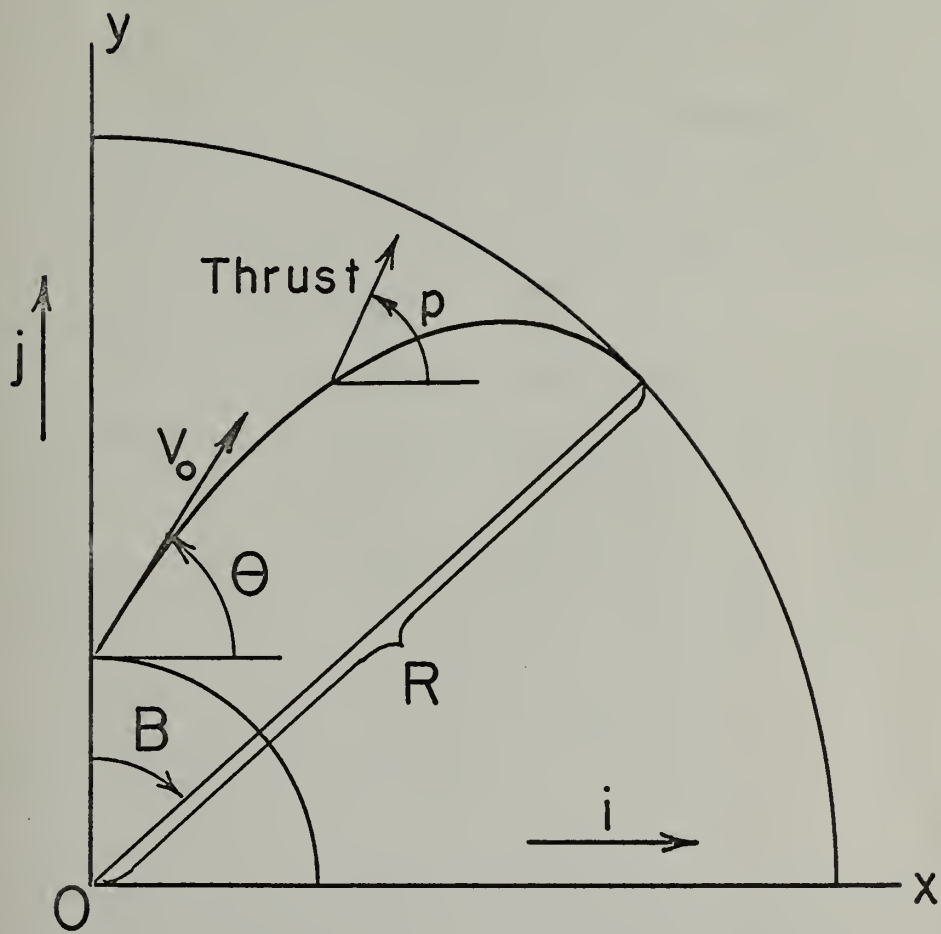


Fig. 1. Orbital transfer.

earth's equatorial radius, $R_e = 20,925,000$ feet. The unit taken for time t is the time required by a hypothetical earth satellite, in equatorial, circular, vacuum, sea level orbit, to traverse a sector of one radian. This unit of time is $\sqrt{R_e/g} = 13.459$ minutes, where $g = 32.086 \text{ ft./sec.}^2$ is the acceleration of gravity at the equator. The unit of velocity is then the speed of this hypothetical satellite. These units of length and time will always be understood, unless other, more conventional units are specifically mentioned.

2. Statement of the problem. The equations of motion of the rocket, in terms of the specified units of length and time, are

$$\begin{aligned}
 (1) \quad \varphi_1 &= \dot{u} - g_1 - a \cos p = 0 \\
 \varphi_2 &= \dot{v} - g_2 - a \sin p = 0 \\
 \varphi_3 &= \dot{x} - u = 0 \\
 \varphi_4 &= \dot{y} - v = 0
 \end{aligned}$$

where $g_1 = -x/r^3$, $g_2 = -y/r^3$, $r^2 = x^2 + y^2$, $a = c\dot{m}/g(1 - \dot{m}t)$, where \dot{m} is the constant fraction of initial gross rocket mass lost per unit of time, c is the constant speed of the emitted rocket gases, and g is the acceleration of gravity at the equator. The fixed initial conditions of the rocket trajectory are taken as

$$\begin{aligned}
 (2) \quad x(0) &= 0, \quad u(0) = V_1 = V_0 \cos \theta \\
 y(0) &= 1, \quad v(0) = V_2 = V_0 \sin \theta.
 \end{aligned}$$

The terminal point of the rocket trajectory is variable with

$$(3) \quad x(T) = X(T), \quad y(T) = Y(T), \quad u(T) = U(T), \quad v(T) = V(T).$$

It is also assumed that the rocket thrust is turned off abruptly at time T . This discontinuity will lead to a trivial steering corner in the calculus of variations problem. Note that (1) and (3) imply that $\dot{U}(T) = -[X/R^3]_T = g_1(T)$ and $\dot{V}(T) = -[Y/R^3]_T = g_2(T)$ where $R = |\vec{i} X + \vec{j} Y|$.

The problem is to choose the control variable p to effect orbital transfer with $\int_0^T dt$ minimized, and to determine the corresponding rocket trajectory. This problem is equivalent to the Lagrange calculus of variations problem of requiring the integral

$$(4) \quad I = \int_0^T (1 + \lambda\varphi_1 + \mu\varphi_2 + \pi\varphi_3 + \rho\varphi_4) dt$$

to be stationary. In (4) the equations (1) are regarded as constraints with $\lambda(t)$, $\mu(t)$, $\pi(t)$, $\rho(t)$ introduced as continua of Lagrangian multipliers [1]. If the time coordinate of the varied terminal point is taken as $T + \Delta T$, the vanishing first variation [2] of I is

$$(5) \quad \delta I = \int_0^T [\lambda(\delta\dot{u} - g_{1x}\delta x - g_{1y}\delta y + a \sin p \delta p) + \pi(\delta\dot{x} - \delta u) + \mu(\delta\dot{v} - g_{2x}\delta x - g_{2y}\delta y - a \cos p \delta p) + \rho(\delta\dot{y} - \delta v)] dt + \int_T^{T+\Delta T} [1 + \lambda\delta\dot{u} + \mu\delta\dot{v} - (\lambda \cos p + \mu \sin p)\delta a] dt = 0$$

where the finite variation δa , $\delta \dot{u}$, $\delta \dot{v}$ terms in the integral from T to $T + \Delta T$, created by thrust termination at time T on the unvaried trajectory and at $T + \Delta T$ on the varied trajectory, cancel.

On integrating by parts one obtains

$$(6) \quad \delta I = [\lambda \delta u + \mu \delta v + \pi \delta x + \rho \delta y]_T - \int_0^T [(\dot{\lambda} + \pi) \delta u + (\dot{\mu} + \rho) \delta v + (\dot{\pi} + g_{1x} \lambda + g_{2x} \mu) \delta x + (\dot{\rho} + g_{1y} \lambda + g_{2y} \mu) \delta y + a(\mu \cos p - \lambda \sin p) \delta p] dt + \Delta T = 0.$$

The variations of the dependent coordinates at the variable terminal point must be taken [2] as

$$(7) \quad \begin{aligned} \delta u(T) &= (\dot{U} - \dot{u})_T \Delta T = -(a \cos p)_T \Delta T, & \delta x(T) &= (\dot{X} - \dot{x})_T \Delta T = 0 \\ \delta v(T) &= (\dot{V} - \dot{v})_T \Delta T = -(a \sin p)_T \Delta T, & \delta y(T) &= (\dot{Y} - \dot{y})_T \Delta T = 0. \end{aligned}$$

Substitution of (7) into (6), and application of the fundamental lemma of the calculus of variations and the theory of ordinary extrema, gives the Euler equations

$$(8) \quad \begin{aligned} \dot{\lambda} + \pi &= 0 \\ \dot{\mu} + \rho &= 0 \\ \dot{\pi} + g_{1x} \lambda + g_{2x} \mu &= 0 \\ \dot{\rho} + g_{1y} \lambda + g_{2y} \mu &= 0 \\ \tan p &= \mu / \lambda \end{aligned}$$

and the transversality condition

$$[a(\lambda \cos p + \mu \sin p)]_T = 1.$$

The first four homogeneous equations of the Euler equations (8) constitute the adjoint system [3] of the system of variation equations

$$(10) \quad \delta\varphi_1 = \delta\varphi_2 = \delta\varphi_3 = \delta\varphi_4 = 0$$

which are the coefficients of λ, μ, π, ρ in (5) equated to zero. The adjoint system has a matrix of coefficients which is the negative transpose of that of (10). The last of the Euler equations (8) requires that the control variable p be adjusted so that $\vec{a} = a(\vec{i} \cos p + \vec{j} \sin p)$, which is proportional to the rocket thrust, is continually parallel to the adjoint vector $\vec{\Lambda} = \vec{i} \lambda + \vec{j} \mu$. The transversality condition (9), which may be written $(\vec{a} \cdot \vec{\Lambda})_T = 1 > 0$, requires that \vec{a} and $\vec{\Lambda}$ have the same sense. Since it is only the ratio of μ to λ which determines p , it is a trivial matter to scale them to satisfy the magnitude requirement of (9).

A solution of the problem obtained from (1) and (8) guarantees a stationary time of transfer. The nature of the problem is such that this stationary time is a minimum time.

3. Numerical solution. There is a constructive aspect of a modification of equation (6), first used by Bliss [4] in his work on differential corrections in ballistics, and applied recently by Faulkner [5] in an iterative fashion in optimum control problems. To find the desired modification of (6), assume that a solution of the systems (1) and (8) has been obtained, which does not necessarily satisfy the terminal conditions (3). Using this

solution and holding T constant, consider the variation of the vanishing integral

$$(11) \quad \int_0^T (\lambda \varphi_1 + \mu \varphi_2 + \pi \varphi_3 + \rho \varphi_4) dt = 0$$

with the terminal constraints (3) removed, so that the terminal variations $\delta u(T)$, $\delta v(T)$, $\delta x(T)$ and $\delta(T)$ become free. Since λ , μ , π , ρ satisfy the adjoint system, and since there is now no steering corner due to thrust termination, one obtains

$$(12) \quad [\lambda \delta u + \mu \delta v + \pi \delta x + \rho \delta y]_T = \int_0^T a(-\lambda \sin p + \mu \cos p) \delta p dt \\ = \int_0^T \vec{\lambda} \cdot (\partial \vec{a} / \partial p) \delta p dt$$

where $\vec{a} = a(\vec{i} \cos p + \vec{j} \sin p)$. Equation (12), which is the desired modification of (6), is called the fundamental formula by Bliss [4], but is also known under the generic name of Green's formula [3]. By the use of (12) it is possible to generate the control parameters of a varied trajectory which, hopefully, comes closer to satisfying the desired terminal conditions (3). To do this, assume that the adjoint system has been solved to obtain a fundamental set of four linearly independent solutions given by the rows of

$$(13) \quad \text{Transpose of } B(t) = [\lambda_i(t) \mu_i(t) \pi_i(t) \rho_i(t)] \quad i = 1, 2, 3, 4$$

where $B(0) = I$ is the identity matrix. The solution $\vec{\lambda} = \vec{i} \lambda + \vec{j} \mu$ of the adjoint system, required to satisfy the last of the Euler

equations (8), is taken as the linear combination

$$(14) \quad \begin{aligned} \lambda &= \lambda_1 + l\lambda_2 + m\lambda_3 + n\lambda_4 \\ \mu &= \mu_1 + l\mu_2 + m\mu_3 + n\mu_4 \end{aligned}$$

so that the control angle p is determined by

$$(15) \quad \tan p = (\mu_1 + l\mu_2 + m\mu_3 + n\mu_4) / (\lambda_1 + l\lambda_2 + m\lambda_3 + n\lambda_4)$$

and its variation by

$$(16) \quad \delta p = [(\lambda\mu_2 - \mu\lambda_2)\delta l + (\lambda\mu_3 - \mu\lambda_3)\delta m + (\lambda\mu_4 - \mu\lambda_4)\delta n] / (\lambda^2 + \mu^2).$$

When (13) and (16) are substituted into (12) there results the system of Green's formulae

$$(17) \quad [\delta u \quad \delta v \quad \delta x \quad \delta y]_T B(T) = [0 \quad \delta l \quad \delta m \quad \delta n] A$$

where the elements of the matrix A are

$$(18) \quad a_{ij} = \int_0^T a(\lambda\mu_i - \mu\lambda_i)(\lambda\mu_j - \mu\lambda_j) dt / (\lambda^2 + \mu^2)^{3/2}.$$

The coordinates of the terminal point of the varied trajectory at time $T + \Delta T$ may be taken as $[u+\Delta u \quad v+\Delta v \quad x+\Delta x \quad y+\Delta y]_T$ where

$$(19) \quad [\Delta u \quad \Delta v \quad \Delta x \quad \Delta y]_T = [\delta u \quad \delta v \quad \delta x \quad \delta y]_T + [\dot{u} \quad \dot{v} \quad \dot{x} \quad \dot{y}]_T \Delta T.$$

In an effort to make this new terminal point come closer to satisfying the terminal conditions (3), one may take

$$(20) \quad [\Delta u \quad \Delta v \quad \Delta x \quad \Delta y]_T = [U-u \quad V-v \quad X-x \quad Y-y]_T + [\dot{U} \quad \dot{V} \quad \dot{X} \quad \dot{Y}]_T \Delta T.$$

Substitute (19) and (20) into (17) to obtain

$$(21) [\dot{U}-\dot{u} \quad \dot{V}-\dot{v} \quad \dot{X}-\dot{x} \quad \dot{Y}-\dot{y}]_T \Delta T + [0 \quad \delta l \quad \delta m \quad \delta n] A B^{-1}(T) = [U-u \quad V-v \quad X-x \quad Y-y]_T$$

as the system of equations for the determination of ΔT , δl , δm , δn on the varied trajectory. The Faulkner [5] scheme for the numerical solution of optimum control problems may now be stated: Make an initial guess for the values of T , l , m , n ; carry out a simultaneous numerical integration of the systems (1), (8) and (18) using the control variable of (15); solve the system (21) for ΔT and the changes in the control parameters; iterate until convergence is obtained. This program may be carried out in a matter of seconds on modern digital computers.

To give an example of this control optimization in the present problem a circular satellite orbit was assumed of radius $R = |\vec{i} X + \vec{j} Y| = 1.075699$, corresponding to an altitude of 300 statute miles above sea level. For this orbit $|\vec{i} U + \vec{j} V| = 1/\sqrt{R}$ and $|\vec{i} \dot{U} + \vec{j} \dot{V}| = 1/R^2$. The assumed rocket launching velocity was $V_0 = |\vec{i} V_1 + \vec{j} V_2| = 0.585402$, launch angle $\theta = 0.928084$ and rendezvous sector $B = 0.153840$ as in Figure 1. Also assumed were $c = 10000.9$ ft./sec. and $\dot{m} = 0.00360583$ sec.⁻¹ The odd appearance of these figures is related to the difficulty, explained in the next section, of obtaining the initial "guesses" $T = 0.289725$, $l = -0.223125$, $m = -29.9875$ and $n = 19.0847$. With this input the process converged in four iterations to the seven significant

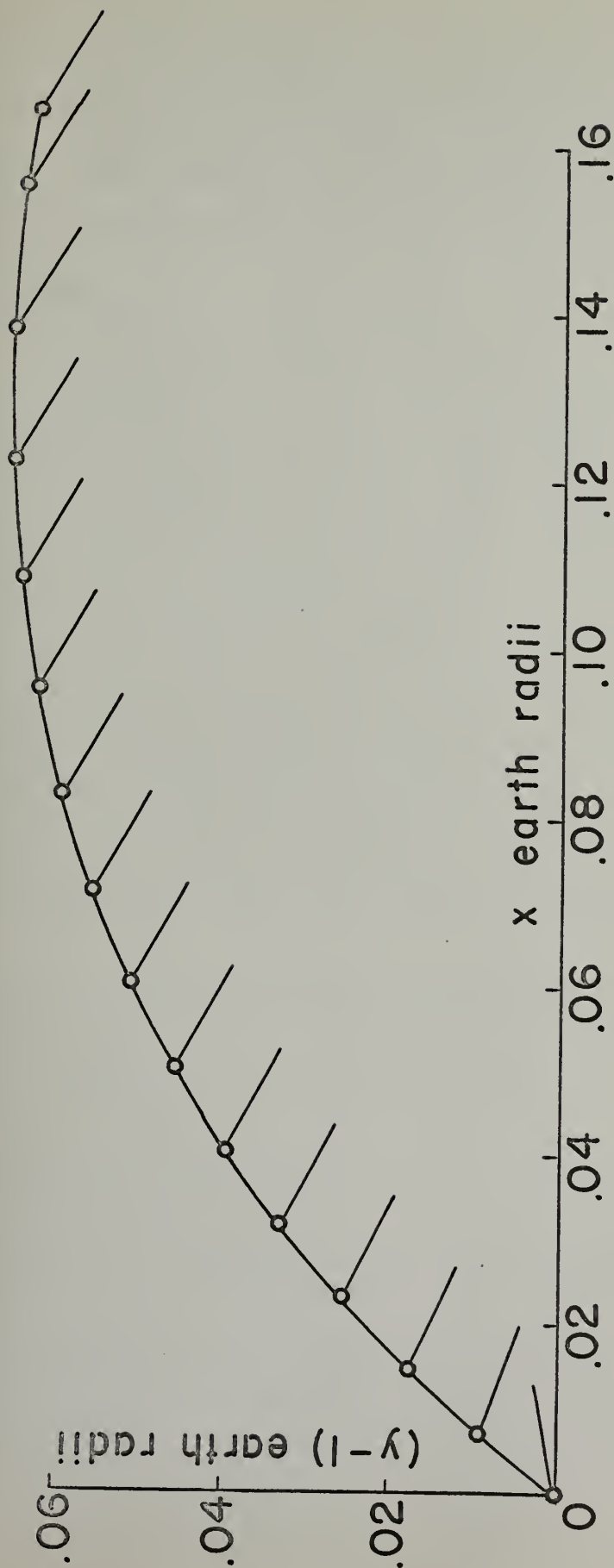


Fig. 2. Trajectory and thrust directions.

figure results $T = 0.2894592$, $l = 0.1840054$, $m = -108.94383$, $n = 67.95886$ and $B = 0.1536015$. Figure 2 shows the resulting trajectory and rocket thrust directions for equal time intervals, excepting the interval terminating in transfer, which is reduced by one half.

4. The initial guesses. The domain of convergence of the iteration scheme of the last section appears to be rather limited in the present control problem, requiring initial guesses for T , l , m , n which make $[U-u \ V-v \ X-x \ Y-y]_T$ small in (21). In the numerical example given here, where the angle B is small and radius R nearly unity, the equations (1) can be linearized and an exact solution of the linearized transfer problem used to supply the input guesses required to solve the non-linear problem. The gravitational terms g_1 and g_2 of (1) were replaced by the linear terms in their Taylor expansions at $x = 0$, $y = 1$. The systems (1) and (8) then become uncoupled. Their solutions, using (2), are

(22)

$$\begin{aligned}
 x &= \int_0^t a \cos p \sin (t-w)dw + V_1 \sin t \\
 u &= \int_0^t a \cos p \cos (t-w)dw + V_1 \cos t \\
 \sqrt{2}y &= \int_0^t a \sin p \sinh \sqrt{2}(t-w)dw + V_2 \sinh \sqrt{2}t - (1/\sqrt{2})\cosh \sqrt{2}t + 3/\sqrt{2} \\
 v &= \int_0^t a \sin p \cosh \sqrt{2}(t-w)dw + V_2 \cosh \sqrt{2}t - (1/\sqrt{2})\sinh \sqrt{2}t \\
 \tan p &= [1 \cosh \sqrt{2}t - (n/\sqrt{2})\sinh \sqrt{2}t]/(\cos t - m \sin t).
 \end{aligned}$$

It will be of no avail to attempt to solve (22) and (3) for T, l, m, n by the Newton-Raphson method, since the Newton-Raphson equations are in fact the system (21) of the poorly convergent iterative routine of the last section. A substitute procedure of solving (22) and (3) for V_1, V_2, \dot{m} and B was used. When the transfer problem has been solved for a sufficient number of such sets (V_1, V_2, \dot{m}, B) , a basis will be at hand for obtaining desired rocket launching conditions by interpolation or extrapolation.

It can now be revealed that the numerical example of the last section really had its genesis in the assumptions $B = \pi/16, \theta = \pi/4, V_0 = 0.65, \dot{m} = 0.0025 \text{ sec.}^{-1}$ and $c = 10000 \text{ ft./sec.}$ It was estimated that $T = 0.3, l = 1.25, m = -1.0$ and $n = 9.5$ would satisfy (22) and (3). Using a cluster of five closely spaced points around (T, l, m, n) , a single application of regula falsi [6] was made in the hope of improving these values of T, l, m, n . The particular cluster chosen gave the output values $T = 0.289725, l = -0.223125, m = -29.9875, n = 19.0847$, which will be recognized as the initial guesses of the last section. The output residuals were $[X-x, Y-y, U-u, V-v]_T = [0.041389, -0.020160, 0.212093, -0.221912]$.

These residuals were then processed by the linear system

$$\begin{aligned}
 (23) \quad (X-x)_T &= \Delta V_1 \sin T - Y(T)dB + \Delta c \int_0^T a \cos p \sin (T-w)dw/c \\
 (U-u)_T &= \Delta V_1 \cos T - V(T)dB + \Delta c \int_0^T a \cos p \cos (T-w)dw/c \\
 \sqrt{2}(Y-y)_T &= \Delta V_2 \sinh \sqrt{2}T + \sqrt{2}X(T)dB + \Delta c \int_0^T a \sin p \sinh \sqrt{2}(T-w)dw/c \\
 (V-v)_T &= \Delta V_2 \cosh \sqrt{2}T + U(T)dB + \Delta c \int_0^T a \sin p \cosh \sqrt{2}(T-w)dw/c,
 \end{aligned}$$

derived from (22) and (3) for the case of a circular orbit, to obtain $c + \Delta c$, launching conditions $V_1 + \Delta V_1$ and $V_2 + \Delta V_2$, and rendezvous sector $B + \Delta B$ which will give small residuals. The value of $c + \Delta c$ turned out to be far from the desired 10000 ft./sec. Instead of changing the value of c , the transformation

$$(24) \quad 10000 \ln [1 - (\dot{m} + \Delta \dot{m})T] = (c + \Delta c) \ln (1 - \dot{m}T),$$

which leaves the integral $\int_0^T a dt$ invariant, was used to change \dot{m} and cause $c + \Delta c$ to approach 10000 ft./sec. on iterating (24), (22) and (23). Seven iterations produced the input values of V_1 , V_2 , c , \dot{m} and B used in the last section.

5. The problem of two fixed end points. The problem in which the conditions at both ends of the rocket trajectory are fixed, or the problem in which rocket and target satellite achieve actual physical rendezvous at a specified angle B , can also be solved by the methods presented here, but with greater convergence difficulties.

Acknowledgement. I am indebted to my colleague, Prof. Frank D. Faulkner, for suggesting the problem of this paper and for discussions of difficulties encountered.

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CDC-1604 ASSEMBLY LANGUAGE COMPUTER PROGRAM

Set content of K100+1 = SLJ 0 L3440 ZRO 0 00000

	REM		COMPUTE LINEARIZED TRAJECTORY
	REM		(B1) = NUMBER OF TRAJECTORIES
	REM		(B4) = NUMBER OF FALSI ITERATIONS LESS ONE
	REM		(A) = FIRST DEPARTURE ANGLE
	REM		(Q) = DELTA DEPARTURE ANGLE
K0	SIL 1	NT	STORE NO. OF TRAJ.
	STA 0	THETATEM	STORE 1ST DEPART ANGLE
	STQ 0	DELTHETA	STORE DELTA DEPART ANGLE
	LDA 0	UNITY	
	FDV 0	R	RECIP. ORBIT RADIUS
	SLJ 4	SQROOT	RET.JUMP TO SQUARE ROOT
	STA 0	V	STORE TARGET SPEED
	FMU 0	V	
	FDV 0	R	
	STA 0	VSQDR	STORE TARGET ACCEL.
	LDA 0	B	TARGET SECTOR AT RENDEVOUS
	SLJ 4	TRIG+70	RET.JUMP TO TRIGONOMETRIC SR.
	STA 0	COSB	
	FMU 0	R	
	STA 0	CAPYFIN	TARGET COOR. AT RENDEVOUS
	LDA 0	B	
K10	SIU 4	K20+6	STORE B4
	SLJ 4	TRIG	
	STA 0	SINB	
	FMU 0	R	
	STA 0	CAPXFIN	TARGET COOR. AT RENDEVOUS
	LDA 0	COSB	
	FMU 0	V	
	STA 0	CAPUFIN	TARGET VEL.COMP. AT RENDEVOUS
	LAC 0	SINB	
	FMU 0	V	
	STA 0	CAPVFIN	TARGET VEL.COMP. AT RENDEVOUS
	LAC 0	COSB	
	FMU 0	VSQDR	
	STA 0	CAPVDFN	TARGET ACC.COMP. AT RENDEVOUS
	LAC 0	SINB	
	FMU 0	VSQDR	
K20	STA 0	CAPUDFN	TARGET ACC.COMP. AT RENDEVOUS
	LDA 0	REARTH	EARTH RADIUS AT EQUATOR
	FDV 0	GACCEL	ACCEL.GRAVITY AT EQUATOR
	SLJ 4	SQROOT	RECIPROCAL SHULER FREQ.
	FMU 0	MDOT	
	STA 0	OMEGA	NON-DIMEN. MASS LOSS RATE
	LDA 0	C	ROCKET NOZZLE VELOCITY
	FMU 0	MDOT	C MDOT
	FDV 0	GACCEL	
	STA 0	A	NON-DIMEN. ACCELERATION
	LDA 0	THETATEM	BEGIN OUTER LOOP
	STA 0	THETA	SET DEPARTURE ANGLE
	ENI 4	0	SET NO. OF FALSI ITERATES
	SLJ 4	TRIG+70	COSINE THETA
	FMU 0	VSTART	
	STA 0	V1	INITIAL HORIZONTAL VELOC.
	LDA 0	THETA	
	SLJ 4	TRIG	SINE THETA
	FMU 0	VSTART	
	STA 0	V2	INITIAL VERTICAL VELOC.
	ENI 3	23	
	ENI 0	0	
	LDA 3	ELIINIT	SET FALSI COOR. QUINTUPLE
	STA 3	EL1	
	IJP 3	/-1	
K30	SLJ 4	70007	PRINT COORS. DECIMAL. B3=0
	STA 0	ELIINIT	PARAMETER WORD

	ZRO 0 T5INIT	
	ENI 5 0	SET B5=0 FOR K40+3
	SLJ 4 700C7	PRINT COORDINATES OCTAL
	ZRO 0 EL1INIT	PARAMETER WORD
K40	ZRO 0 T5INIT	
	SLJ 4 XYUV	SET FALSI FUNC. QUINTUPLE
	ZRO 0 0	
	SLJ 4 70007	PRINT FUNCTIONS DECIMAL
	ZRO 0 0	
	STA 0 DELXFIN	PARAMETER WORD
	ZRO 0 DELVFIN	
	LDA 0 DELXFIN	
	STA 5 DELX1	
	LDA 0 DELYFIN	
	STA 5 DELY1	
	LDA 0 DELUFIN	
	STA 5 DELU1	
	LDA 0 DELVFIN	
	STA 5 DELV1	
	INI 5 5	
	INI 3 3	
K50	ISK 3 23	
	SLJ 0 K40	
	ENI 0 0	BEGIN INNER LOOP OR SLJ.0 K101 OR L3440
	SLJ 4 MATRIX	INVERT DELXYUV MATRIX
	SLS 0 K50+2	SINGULAR MATRIX ALARM HALT
	ZRO 0 0	
	ZRO 0 0	
	ZRO 0 5	CODE TO INVERT = 5
	ZRO 0 5	L = 5 ROWS IN DELXYUV MATRIX
	ZRO 0 DELX1-1	ADD. OF DELXYUV MATRIX = DELX1-1
	ZRO 0 0	N=0. WORD NOT USED
	ZRO 0 0	
	ZRO 0 0	M=0
	ZRO 0 DELX1+174	ADD. OF INVERSE = DELX1+174
	ENI 0 0	
K60	SLJ 4 MATRIX	INVERSE TIMES LMNT MATRIX
	ZRO 0 K60	WORD NOT USED
	ZRO 0 0	
	ZRO 0 0	
	ZRO 0 4	MATRIX MULT. CODE = 4
	ZRO 0 5	L = 5 ROWS IN INVERSE
	ZRO 0 DELX1+174	ADD. OF INVERSE = DELX1+174
	ZRO 0 5	N=5 COLUMNS IN INVERSE
	ZRO 0 EL1	ADDRESS OF LMNT MATRIX = EL1
	ZRO 0 4	M=4 COLS. IN MATRIX PRODUCT
	ZRO 0 EL1+24	ADDRESS OF PROD. = EL1+24
	LDA 3 EL2	SHIFT COORS. AND FUNCS. B3=0
	STA 3 EL1	
	LDA 3 DELX2-1	
	STA 3 DELX1-1	
	ISK 3 23	
	SLJ 0 /-2	
K70	ENI 3 20	
	ENI 5 3	FOR USE IN K70+2
	SLJ 4 XYUV	COMPUTE NEW DELXYUV FUNCS.
	ZRO 0 0	
	LDA 5 DELXFIN	STORE NEW FUNCS.
	STA 5 DELX5	
	IJP 5 /-1	
	SLJ 4 70007	PRINT NEW COORS. DEC. WITH PANEL
	SAU 0 EL5	PARAMETER WORD
	ZRO 0 T5	
	EXF 0 70	CLEAR ARITHMETIC ERRORS
	SLJ 4 70007	PRINT NEW COORS. OCTAL
	ZRO 0 EL5	PARAMETER WORD
	ZRO 0 T5	
	ENI 3 0	CLEAR B3
K100	SLJ 4 70007	PRINT NEW FUNCS. DECIMAL
	STA 0 DELXFIN	PARAMETER WORD

	ZRO 0	DELVFIN	
	IJP 4	K50+1	END INNER LOOP (OR SLJ 0 L3440)
	LDQ 0	EL5	
	LDA 0	UNITY	
	SLJ 4	POLAR+130	
	STQ 0	QQ	DEPARTURE THRUST ANGLE
	ENI 1	2	
	LDA 1	EL5	MOVE EL5, EM5 AND EN5
	STA 1	EL	
	IJP 1	/-1	
	LAC 0	V	(-V)
	FMU 0	TAUFIN	(-VT)
	FDV 0	R	(-VT/R)
	FAD 0	B	B-(VT/R)
K110	STA 0	S	S = INITIAL TARGET SECTOR
	SLJ 4	70007	ALARM REENTRY FROM LOG S.R.
	ZRO 0	0	DECIMAL DUMP WITH PANEL
	SAU 0	CAPXFIN	PARAMETER WORD
	ZRO 0	LAM	
	SLJ 4	70007	DECIMAL DUMP
	ZRO 0	0	
	STA 0	NT	PARAMETER WORD
	ZRO 0	S	
	SLJ 4	70007	OCTAL DUMP
	ZRO 0	0	
	ZRO 0	NT	PARAMETER WORD
	ZRO 0	DELTHETA	
	LDA 0	THETA	
	FAD 0	DELTHETA	
	STA 0	THETATEM	SET NEW THETA
K120	RSO 0	NT	
	AJP 1	K20+5	END OUTER LOOP. (SEE K440)
XYUV	SLS 0	BEGIN	HALT. START RENDEVOUS PROG.
	SLJ 0	0	ENTER DELXYUV SUBROUTINE
	LDA 3	T1	
	STA 0	TAUFIN	
	LAC 0	OMEGA	(-W)
	FMU 0	TAUFIN	(-WT)
	FAD 0	UNITY	
	STA 0	STOR1	(STOR1) = 1 - WT
	FDV 0	OMEGA	
	STA 0	STOR2	(STOR2) = (1-WT)/W
	FMU 0	STOR2	SQUARE
	FMU 0	STOR2	CUBE
	FMU 0	STOR2	FOURTH
	FMU 0	STOR2	FIFTH
K130	FMU 0	ERRCOF	MULT. BY -15.8-12
	FDV 0	TAUFIN	
	STA 0	STOR3	
	LDA 0	STOR1	1-WT
	SLJ 4	LOG+66	LOG(1-WT) TO BASE E
	FMU 0	STOR3	
	SLJ 4	SQROOT	
	SLJ 4	SQROOT	
	ZRO 0	0	
	STA 0	DELTAU	COMPUTED TAU INCREMENT
	SLJ 4	EQUAL	EQUALIZE DELTAU AND SET B2
	STA 0	DELT1	SET EQUALIZED DELT1
	ENA 0	4	
	STA 0	RUNKT1	SET GILL FOR 4 INTEGRALS
	ENI 1	14	
	ENA 0	0	
K140	STA 1	TAU1	CLEAR RUNKT1 AREA
	IJP 1	/-1	
	ENI 0	0	
	LDA 0	TAUFIN	
	SLJ 4	TRIG	SIN T
	STA 0	SINT	
	FMU 0	V1	V1 SINT
	FSB 0	CAPXFIN	V1 SINT - X

	STA 0 DELXFIN	
	LDA 0 TAUFIN	
	SLJ 4 TRIG+70	COS T
	STA 0 COST	
	FMU 0 V1	V1 COST
	FSB 0 CAPUFIN	V1 COST - U
	STA 0 DELUFIN	
	LDA 0 TAUFIN	
K150	FMU 0 ROOT2	T TIMES SQ. ROOT 2
	SLJ 4 EXP+107	
	ZRO 0 0	
	STA 0 COSHTR2	STORE HYP. COSINE
	FMU 0 ROOTHALF	COSHTR2/SQ.ROOT 2
	STA 0 STOR1	
	LDA 0 TAUFIN	
	FMU 0 ROOT2	
	SLJ 4 EXP+71	
	STA 0 SINHTR2	STORE HYP. SINE
	FMU 0 V2	V2 SINHTR2
	FSB 0 STOR1	
	FAD 0 THREDR2	ADD (3/SQ.ROOT 2)
	STA 0 STOR1	
	LAC 0 CAPYFIN	(-Y)
	FMU 0 ROOT2	
	FAD 0 STOR1	
K160	STA 0 DELYFIN	
	LDA 0 COSHTR2	
	FMU 0 V2	
	STA 0 STOR1	(STOR1) = V2 COSHTR2
	LAC 0 SINHTR2	(-SINHTR2)
	FMU 0 ROOTHALF	
	FAD 0 STOR1	
	FSB 0 CAPVFIN	
	STA 0 DELVFIN	
	LDA 3 EL1	
	FMU 3 EL1	EL1 SQUARED
	FAD 0 UNITY	1 + EL1 SQ.
	SLJ 4 SQROOT	
	ZRO 0 0	
	STA 0 HYP	
K170	LDA 0 A	
	FDV 0 HYP	
	STA 0 STOR1	(STOR1) = A/HYP = A COS P
	FMU 0 SINT	
	STA 0 SINDOT	A COSP SINT
	LDA 0 STOR1	A COSP
	FMU 0 COST	
	STA 0 COSDOT	A COSP COST
	LDA 0 STOR1	A/HYP
	FMU 3 EL1	A SINP
	FMU 0 SINHTR2	
	STA 0 SINHDOT	A SINP SINHTR2
	LDA 0 STOR1	A/HYP
	FMU 3 EL1	A SINP
	FMU 0 COSHTR2	
	STA 0 COSHDOT	A SINP COSHTR2
	SLJ 4 ALPHA	SET UP GILL ROUTINE
K200	ZRO 0 RUNKT1	PARAMETER WORD
	ZRO 0 DERIV1	
	IJP 2 /+1	JUMP IF B2 NOT = ZERO
	SLJ 0 /+3	B2=0. END OF INTEGRATION
	ENI 0 0	B2 NOT = ZERO
	SLJ 4 ALPHA+1	INTEGRATE AGAIN
	ENI 0 0	
	SLJ 0 /-2	JUMP TO TEST B2
	LDA 0 DELXFIN	
	FAD 0 SIN	
	STA 0 DELXFIN	
	LDA 0 DELUFIN	
	FAD 0 COS	

	STA 0	DELUFIN	
	LDA 0	DELYFIN	
K210	FAD 0	SINH	
	FDV 0	ROOT2	
	STA 0	DELYFIN	
	LDA 0	DELVFIN	
	FAD 0	COSH	
	STA 0	DELVFIN	
DERIV1	SLJ 0	XYUV	TO EXIT OF SUBROUTINE
	LAC 0	TAU1	
	FMU 0	OMEGA	(-WT)
	FAD 0	UNITY	
	STA 0	UNMINWT	1-WT
	LDA 0	A	
	FDV 0	UNMINWT	
	STA 0	ADOMINWT	A/(1-WT)
	LDA 0	TAUFIN	
	FSB 0	TAU1	
K220	STA 0	STOR1	(STOR1) = TAUFIN - TAU1
	ENI 0	0	
	SLJ 4	TRIG	
	STA 0	SINT	(SINT) = SINE OF (STOR1)
	LDA 0	STOR1	
	SLJ 4	TRIG+70	
	ZRO 0	0	
	STA 0	COST	
	LDA 0	STOR1	
	FMU 0	ROOT2	
	SLJ 4	EXP+71	
	STA 0	SINHTR2	
	LDA 0	STOR1	
	FMU 0	ROOT2	
	SLJ 4	EXP+107	
	STA 0	COSHTR2	
K230	LDA 0	TAU1	SIN TAU1 = -LAM3
	SLJ 4	TRIG	
	ZRO 0	0	
	FMU 3	EM1	
	STA 0	STOR2	(STOR2) = - EM1 LAM3
	LDA 0	TAU1	
	SLJ 4	TRIG+70	COS TAU1 = LAM1
	FSB 0	STOR2	LAM1 + EM1 LAM3
	STA 0	LAM	LAM = LAM1 + EM1 LAM3
	FMU 0	LAM	
	STA 0	STOR3	(STOR3) = LAM SQUARED
	LDA 0	TAU1	
	FMU 0	ROOT2	
	SLJ 4	EXP+71	SINH TAU1R2
	ZRO 0	0	
	FMU 3	EN1	
K240	FDV 0	ROOT2	(- EN1 MU4)
	STA 0	STOR2	(STOR2) = - EN1 MU4
	LDA 0	TAU1	
	FMU 0	ROOT2	
	SLJ 4	EXP+107	COSH TAU1R2 = MU2
	FMU 3	EL1	EL1 MU2
	FSB 0	STOR2	EL1 MU2 + EN1 MU4 = MU
	STA 0	MU	
	FMU 0	MU	
	FAD 0	STOR3	LAM SQ. + MU SQ.
	SLJ 4	SQR00T	
	STA 0	HYP	
	LDA 0	MU	
	FDV 0	HYP	
	STA 0	STOR3	(STOR3) = SINP
	LDA 0	LAM	
K250	FDV 0	HYP	
	STA 0	STOR4	(STOR4) = COSP
	FMU 0	SINT	COSP SINT
	FMU 0	ADOMINWT	

	STA 0	SINDOT	
	LDA 0	STOR4	COSP
	FMU 0	COST	COSP COST
	FMU 0	ADOMINWT	
	STA 0	COSDOT	
	LDA 0	STOR3	SINP
	FMU 0	SINHTR2	SINP SINHTR2
	FMU 0	ADOMINWT	
	STA 0	SINHDOT	
	LDA 0	STOR3	SINP
	FMU 0	COSHTR2	SINP COSHTR2
	FMU 0	ADOMINWT	
K260	STA 0	COSHDOT	
	SLJ 0	ALPHA+2	EXIT FROM DERIVI
	ZRO 0	0	
EQUAL	SLJ 0	0	S.R. TO EQUALIZE DELTAU
	LDA 0	TAUFIN	
	FDV 0	DELTAU	
	SLJ 4	FIXIT	CONVERT DELTAU TO FIXED PT.
	STA 0	INTSIGN	STORE INTEGRAL PART
	STQ 0	FRACSIGN	STORE FRACTIONAL PART
	AJP 1	/+5	JUMP IF A NOT = ZERO
	QJP 0	/+3	A=0. JUMP IF Q = 0
	LDA 0	TAUFIN	A=0. Q NOT = 0
	STA 0	DELTFLSG	
	ENI 2	1	
	SLJ 0	/+12	
	ENA 0	0	A = Q = 0
	STA 0	DELTFLSG	
K270	ENI 2	0	
	SLJ 0	/+10	
	AJP 2	/+1	A NOT 0. JUMP IF A GREATER THAN 0
	SCM 0	MASK	A LESS THAN 0. ABSO INTEGER TO A
	INA 0	1	ABSO. INTEGER + 1 TO A
	SAU 0	/+1	
	ENI 2	0	ABSO. INTEGER + 1 TO B2
	SCA 1	2057	
	LRS 0	57	
	ENA 1	0	
	LLS 0	44	
	STA 0	FLOIPLON	
	LDA 0	TAUFIN	
	FDV 0	FLOIPLON	
	STA 0	DELTFLSG	
	ENI 0	0	
K300	SIL 2	FIXIPLON	USED IN FINAL PROG.
	LDA 0	DELTFLSG	
	SLJ 0	EQUAL	TO EXIT OF S.R.
	ZRO 0	0	
FIXIT	BSS	44	B1=5 B6=65302 P=460
R	DEC	1.075698925	NON-DIMEN. ORBIT RADIUS
V	BSS	1	NON-DIMEN. TARGET SPEED
VSQDR	BSS	1	NON-DIMEN. TARGET ACCEL.
B	OCT	1775622077325042	TARGET SECTOR AT RENDEVOUS = PI/16
COSB	BSS	1	
SINB	BSS	1	
REARTH	DEC	20925000.	EARTH EQUATOR RAD. IN FT.
GACCEL	DEC	32.086	EQUATOR GRAVITY IN FT/SEC/SEC
RMS	BSS	1	
OMEGA	BSS	1	NON-DIMEN. MASS LOSS RATE
THETATEM	BSS	1	
V1	BSS	1	NON-DIMEN. INIT. HORIZONTAL VEL.
V2	BSS	1	NON-DIMEN. INIT. VERTICAL VEL.
ERRCOF	DEC	-15.B-12	(-15/4096 DEC.) USED TO FIND DELTAU
ROOTHALF	OCT	2000552023631500	
SINT	BSS	1	
COST	BSS	1	
SINHTR2	BSS	1	
COSHTR2	BSS	1	
UNMINWT	BSS	1	STORE FOR (1-WT)

EL1INIT	OCT	2001500400000000	DEC.VALUE = +1.251953125
EM1INIT	OCT	5776377777777777	DEC.VALUE = -1.000000000
EN1INIT	OCT	2004460000000000	DEC.VALUE = +9.500000000
T1INIT	OCT	1776463146314631	DEC.VALUE = +0.300000000
EL2INIT	OCT	2001500300000000	DEC.VALUE = +1.251464844
EM2INIT	OCT	5776377777777777	DEC.VALUE = -1.000000000
EN2INIT	OCT	2004460100000000	DEC.VALUE = +9.503906250
T2INIT	OCT	1776461700000000	DEC.VALUE = +0.2987060547
EL3INIT	OCT	2001500200000000	DEC.VALUE = +1.250976562
EM3INIT	OCT	5776377777777777	DEC.VALUE = -1.000000000
EN3INIT	OCT	2004460200000000	DEC.VALUE = +9.507812500
T3INIT	OCT	1776462000000000	DEC.VALUE = +0.2988281250
EL4INIT	OCT	2001500100000000	DEC.VALUE = +1.250488281
EM4INIT	OCT	57763777707007777	DEC.VALUE = -1.000434756
EN4INIT	OCT	2004460300000000	DEC.VALUE = +9.511718750
T4INIT	OCT	1776464300000000	DEC.VALUE = +0.3011474609
EL5INIT	OCT	2001500000000000	DEC.VALUE = +1.250000000
EM5INIT	OCT	5776377777077077	DEC.VALUE = -1.000006689
EN5INIT	OCT	2004460400000000	DEC.VALUE = +9.515625000
T5INIT	OCT	1776465000000000	DEC.VALUE = +0.3017578125
RUNKT1	BSS	1	
DELT1	BSS	1	
TAU1	BSS	1	
SINDOT	BSS	1	
SIN	BSS	2	
COSDOT	BSS	1	
COS	BSS	2	
SINHDOT	BSS	1	
SINH	BSS	2	
COSHDOT	BSS	1	
COSH	BSS	3	
K440	ENI	3 23	RESET LMNT INIT. (SEE K120)
	ENI	0 0	
	LDA	3 EL1	
	STA	3 EL1INIT	
	IJP	3 /-1	
	LDA	0 NT	
	AJP	1 K20+5	
	SLS	0 BEGIN	HALT. START RENDEVOUS PROG.
	BSS	3	
EXP	BSS	117	B1=3 B6=65447 P=460
SQROOT	BSS	65	B1=6 B6=65566 P=460
TRIG	BSS	116	B1=7 B6=65653 P=460
ADMINWT	BSS	1	STORE FOR A/(1-WT)
ROOT2	OCT	2001552023631500	
TWO	OCT	2002400000000000	
THREE	OCT	2002600000000000	
MASK	OCT	7777777777777777	
TENGRAND	DEC	100C0.	
COMPRMS	OCT	1754400000000000	
	REM		RENDEVOUS PROG. STARTS HERE
BEGIN	ENI	6 12	SET NUMBER OF ITERATIONS
	ENI	0 0	
	ENI	0 0	
	ENI	0 0	
	LDA	0 V	
	FDV	0 R	V/R = W
	STA	0 W	STORE TARGET ANGULAR VEL.
	ENI	0 0	
	ENI	0 0	
	ENI	0 0	
	ENI	0 0	
	ENA	0 35	
	STA	0 RUNKT	SET GILL S.R. FOR 29 DIFF.EQUS.
	ENI	0 0	
	ENI	0 0	
	ENI	1 0	
L10	ENA	0 0	CLEAR RUNKT+17 AREA
	STA	1 RUNKT+17	

	STA 1	RUNKT+20	
	INI 1	2	
	ISK 1	112	
	SLJ 0	/-2	
	LDA 0	UNITY	
	STA 0	RUNKT+20	SET LAM1(0)=1
	STA 0	RUNKT+37	SET MU2(0)=1
	STA 0	RUNKT+56	SET PI3(0)=1
	STA 0	RUNKT+75	SET RH04(0)=1
	STA 0	RUNKT+25	SET PI1DOT(0)=1
	LAC 0	UNITY	
	STA 0	RUNKT+47	SET LAM3DOT(0)=-1
	STA 0	RUNKT+66	SET MU4DOT(0)=-1
	LAC 0	TWO	
L20	STA 0	RUNKT+44	SET RH02DOT(0)=-2
	ENI 0	0	
	ENI 0	0	
	ENI 0	0	
	ENI 0	0	
	ENA 0	0	
	STA 0	RUNKT+2	SET TAU = 0
	STA 0	RUNKT+4	SET X(0)=0
	LDA 0	V1	
	STA 0	RUNKT+3	SET XDOT(0)=V1
	STA 0	RUNKT+12	SET U(0)=V1
	LDA 0	V2	
	STA 0	RUNKT+6	SET YDOT(0)=V2
	STA 0	RUNKT+15	SET V(0)=V2
	LDA 0	UNITY	
	STA 0	RUNKT+7	SET Y(0)=1
L30	ENI 0	0	
RECUR	SLJ 0	/+5	BYPASS
	SIU 6	/+1	
	SLS 1	/+1	STOP SWITCH
	ENI 6	0	
	ENI 1	147	
	LDA 1	SAVE	
	STA 1	RUNKT	
	IJP 1	/-1	
	ENI 0	0	
	SLJ 4	EQUAL	
	ZRO 0	0	
	STA 0	RUNKT+1	STORE EQUALIZED DELTAU
	SLJ 4	LAMMU	RET.JUMP TO OBTAIN LAM AND MU
	SLJ 0	L70	BYPASS LAMMU
LAMMU	ZRO 0	0	
	SLJ 0	0	ENTRANCE TO S.R.
	SIL 1	L60+3	SAVE B1
	SIU 3	L60+4	SAVE B3
	LDA 0	RUNKT+20	LOAD LAM1
	STA 0	STOR3	LAM1 TO STOR3
	ENI 0	0	
	ENI 1	0	SET B1=0
	ENI 3	0	SET B3=0
	LDA 1	EL	
	FMU 3	RUNKT+34	EL(LAM2)
	FAD 0	STOR3	
	STA 0	STOR3	
	INI 3	14	
	ENI 0	0	
	ISK 1	2	
L50	SLJ 0	/-3	
	STA 0	LAM	STORE LAMBDA
	FMU 0	LAM	LAM SQUARED
	STA 0	STOR1	LAM SQUARE TO STOR 1
	LDA 0	RUNKT+23	LOAD MU1
	STA 0	STOR3	
	ENI 3	0	
	LDA 1	EL	
	FMU 3	RUNKT+37	EL(MU2)

	FAD 0	STOR3	
	STA 0	STOR3	
	INI 3	14	
	ENI 0	0	
	ISK 1	2	
	SLJ 0	7-3	
	STA 0	MU	STORE MU
	FMU 0	MU	MU SQUARED
L60	FAD 0	STOR1	LAM SQ + MU SQ
	STA 0	HYP2	HYP2 = LAM SQ + MU SQ
	SLJ 4	SQROOT	
	ZRO 0	0	
	STA 0	HYP	HYP = SQ ROOT OF HYP2
	FMU 0	HYP2	
	STA 0	HYP3	HYP3 = HYP2 TIMES HYP
	ENI 1	0	RESTORE B1
	ENI 3	0	RESTORE B3
	SLJ 0	LAMMU	TO EXIT OF S.R.
	BSS 3		
L70	LDA 0	A	ENTER FROM L30+7
	FMU 0	LAM	
	FDV 0	HYP	
	STA 0	RUNKT+11	SET UDOT(0) = A(LAM)/HYP
	LDA 0	A	
	FMU 0	MU	
	FDV 0	HYP	
	FSB 0	UNITY	
	STA 0	RUNKT+14	SET VDOT(0)
	ENA 0	7+2	CURRENT ADDRESS+2 TO A
	SAL 0	L220-4	SET EXIT FROM DERIV. PROG.
	SLJ 0	L150-3	JUMP TO SET AIJDOT(0)
	ENA 0	ALPHA+2	
	SAL 0	L220-4	REPAIR EXIT FROM DERIV.PROG.
	ENI 0	0	
	SLJ 0	L220-3	BYPASS DERIV. PROG.
DERIV	LAC 0	OMEGA	
	FMU 0	RUNKT+2	(-WT)
	FAD 0	UNITY	1-WT
	STA 0	UNMINWT	STORE (1-WT)
	LDA 0	A	
	FDV 0	UNMINWT	
	STA 0	ADOMINWT	STORE A/(1-WT)
	ENI 0	0	
	LDA 0	RUNKT+12	
	STA 0	RUNKT+3	SET XDOT = U
	LDA 0	RUNKT+15	
	STA 0	RUNKT+6	SET YDOT = V
	LDA 0	RUNKT+4	LOAD X
	FMU 0	RUNKT+4	X SQUARED
	STA 0	STOR2	X SQ TO STOR2
	LDA 0	RUNKT+7	LOAD Y
L110	FMU 0	RUNKT+7	Y SQUARED
	FAD 0	STOR2	X SQ + Y SQ
	STA 0	STOR1	(X SQ + Y SQ) TO STOR1
	SLJ 4	SQROOT	
	FMU 0	STOR1	
	STA 0	R32	STORE RADIUS CUBED
	FMU 0	STOR1	
	STA 0	R52	STORE RADIUS FIFTH
	ENI 1	0	
	SLJ 4	LAMMU	NOTE B1 SAVED BY LAMMU
	LAC 1	RUNKT+4	(-X) TO A
	FDV 0	R32	
	STA 0	STOR1	(-X/R32) TO STOR1
	LDA 0	ADOMINWT	
	FMU 1	LAM	
	FDV 0	HYP	
L120	FAD 0	STOR1	
	STA 1	RUNKT+11	SET UDOT(T)
	INI 1	2	

	ENI	0	0	
	ISK	1	5	
	SLJ	0	L120-3	
	ENI	0	0	
	ENI	3	0	
	LAC	3	RUNKT+26	(-PI1)
	STA	3	RUNKT+17	SET LAM1DOT = -PI1
	LAC	3	RUNKT+31	(-RHO1)
	STA	3	RUNKT+22	SET MU1DOT = -RHO1
	LDA	0	RUNKT+7	Y
	FMU	0	RUNKT+7	Y SQUARED
	FSB	0	STOR2	Y SQ - X SQ
	FSB	0	STOR2	Y SQ - 2(X SQ)
L130	FMU	3	RUNKT+20	(Y SQ - 2 X SQ)LAM1
	STA	0	STOR1	
	LAC	0	THREE	MINUS THREE
	FMU	0	RUNKT+4	(-3X)
	FMU	0	RUNKT+7	(-3XY)
	FMU	3	RUNKT+23	(-3XY MU1)
	FAD	0	STOR1	
	FDV	0	R52	
	STA	3	RUNKT+25	SET PI1DOT
	LAC	0	RUNKT+7	(-Y)
	FMU	0	RUNKT+7	(- Y SQUARED)
	FMU	0	TWO	(-2 Y SQUARED)
	FAD	0	STOR2	X SQ - 2 Y SQ
	FMU	3	RUNKT+23	(X SQ - 2 Y SQ)MU1
	STA	0	STOR1	
	LAC	0	THREE	MINUS THREE
L140	FMU	0	RUNKT+4	(-3X)
	FMU	0	RUNKT+7	(-3XY)
	FMU	3	RUNKT+20	(-3XY LAM1)
	FAD	0	STOR1	
	FDV	0	R52	
	STA	3	RUNKT+30	SET RHO1DOT
	INI	3	13	
	ENI	0	0	
	ISK	3	57	
	SLJ	0	L130-4	
	LAC	0	OMEGA	(-W). ENTER FROM L70+5
	FMU	0	RUNKT+2	(-WT)
	FAD	0	UNITY	1-WT
	STA	0	UNMINWT	
	LDA	0	A	LOAD INITIAL ACCEL.
	FDV	0	UNMINWT	A/(1-WT)
L150	STA	0	ADOMINWT	
	ENI	0	0	
	LAC	0	MU	
	FMU	0	RUNKT+20	(-MU LAM1)
	STA	0	STOR1	
	LDA	0	LAM	
	FMU	0	RUNKT+23	LAM MU1
	FAD	0	STOR1	
	STA	0	A1	A1 = LAM MU1 - MU LAM1
	LAC	0	MU	
	FMU	0	RUNKT+34	(-MU LAM2)
	STA	0	STOR1	
	LDA	0	LAM	
	FMU	0	RUNKT+37	LAM MU2
	FAD	0	STOR1	
	STA	0	A2	A2 = LAM MU2 - MU LAM2
L160	FMU	0	A1	A1 TIMES A2
	FMU	0	ADOMINWT	(A/(1-WT))A1A2
	FDV	0	HYP3	
	STA	0	RUNKT+77	SET A12DOT
	LAC	0	MU	
	FMU	0	RUNKT+50	(-MU LAM3)
	STA	0	STOR1	
	LDA	0	LAM	
	FMU	0	RUNKT+53	LAM MU3

	FAD	0	STOR1	
	STA	0	A3	A3 = LAM MU3 - MU LAM3
	FMU	0	A1	A1 TIMES A3
	FMU	0	ADOMINWT	
	FDV	0	HYP3	
	STA	0	RUNKT+102	SET A13DOT
L170	LAC	0	MU	
	FMU	0	RUNKT+64	(-MU LAM4)
	STA	0	STOR1	
	LDA	0	LAM	
	FMU	0	RUNKT+67	LAM MU4
	FAD	0	STOR1	
	STA	0	A4	A4 = LAM MU4 - MU LAM4
	FMU	0	A1	A1 TIMES A4
	FMU	0	ADOMINWT	
	FDV	0	HYP3	
	STA	0	RUNKT+105	SET A14DOT
	LDA	0	A2	
	FMU	0	A2	A2 SQUARED
	FMU	0	ADOMINWT	
	FDV	0	HYP3	
	STA	0	RUNKT+110	SET A22DOT
L200	LDA	0	A2	
	FMU	0	A3	A2 TIMES A3
	FMU	0	ADOMINWT	
	FDV	0	HYP3	
	STA	0	RUNKT+113	SET A23DOT
	LDA	0	A2	
	FMU	0	A4	A2 TIMES A4
	FMU	0	ADOMINWT	
	FDV	0	HYP3	
	STA	0	RUNKT+116	SET A24DOT
	LDA	0	A3	
	FMU	0	A3	A3 SQUARED
	FMU	0	ADOMINWT	
	FDV	0	HYP3	
	STA	0	RUNKT+121	SET A33DOT
	LDA	0	A3	
L210	FMU	0	A4	A3 TIMES A4
	FMU	0	ADOMINWT	
	FDV	0	HYP3	
	STA	0	RUNKT+124	SET A34DOT
	LDA	0	A4	
	FMU	0	A4	A4 SQUARED
	FMU	0	ADOMINWT	
	FDV	0	HYP3	
	STA	0	RUNKT+127	SET A44DOT
	ENI	0	0	
	SLJ	0	ALPHA+2	END OF DERIV PROG.
	ENI	0	0	ENTER FROM L70+7
	ENI	1	147	
	LDA	1	RUNKT	STORE INIT. CONDITIONS
	STA	1	SAVE	FOR NEXT ITERATE
	IJP	1	/-1	
L220	SLJ	4	ALPHA	SET UP GILL ROUTINE
	ZRO	0	RUNKT	PARAMETER WORD
	ZRO	0	DERIV	
	IJP	2	/+1	JUMP IF B2 NOT = ZERO
	SLJ	0	/+3	B2=0. JUMP TO RMS COMP.
	ENI	0	0	B2 NOT = ZERO
	SLJ	4	ALPHA+1	INTEGRATE AGAIN
	ENI	0	0	
	SLJ	0	/-2	JUMP TO TEST B2
	LDA	0	CAPXFIN	BEGIN R.M.S. COMPUTATION
	FSB	0	RUNKT+4	CAPXFIN - XFIN
	STA	0	C3	
	FMU	0	C3	
	STA	0	STOR2	
	LDA	0	CAPYFIN	
	FSB	0	RUNKT+7	CAPYFIN - YFIN

L230	STA 0 C4	
	FMU 0 C4	
	FAD 0 STOR2	
	STA 0 STOR2	
	LDA 0 CAPUFIN	
	FSB 0 RUNKT+12	CAPUFIN - UFIN
	STA 0 C1	
	FMU 0 C1	
	FAD 0 STOR2	
	STA 0 STOR2	
	LDA 0 CAPVFIN	
	FSB 0 RUNKT+15	CAPVFIN - VFIN
	STA 0 C2	
	FMU 0 C2	
	FAD 0 STOR2	
	SLJ 4 SQR00T	
	ZRO 0 0	
L240	FDV 0 TWO	
	STA 0 RMS	STORE ROOT MEAN SQUARE
	ENI 1 17	
	ENI 3 55	
	LDA 3 RUNKT+20	SET 4 BY 4 MATRIX
	STA 1 BB11	LAMIMUIPIIRHOI = B
	INI 3 -3	(I=1,2,3,4) AT TAUFIN
	IJP 1 /-1	
	SLJ 4 MATRIX	INVERT THE MATRIX
	ZRO 0 0	
	SLS 0 L250-3	SINGULAR MATRIX ALARM HALT
	ZRO 0 0	
	ZRO 0 0	
	ZRO 0 5	CODE TO INVERT = 5
	ZRO 0 4	L = 4
L250	ZRO 0 BB11	BB11 = ADDRESS OF B MATRIX
	ZRO 0 0	N=0 NOT USED IN INVERT
	ZRO 0 0	
	ZRO 0 0	M=0 NOT USED IN INVERT
	ZRO 0 BB11+120	BB11+120 = ADDRESS OF INVERSE
	LDA 0 RUNKT+100	A12 TO SET 4 BY 3 D MATRIX
	STA 0 BB11+100	SET D11 = A12
	LDA 0 RUNKT+103	A13
	STA 0 BB11+101	SET D12 = A13
	LDA 0 RUNKT+106	A14
	STA 0 BB11+102	SET D13 = A14
	LDA 0 RUNKT+111	A22
	STA 0 BB11+103	SET D21 = A22
	LDA 0 RUNKT+114	A23
	STA 0 BB11+104	SET D22 = A23
	STA 0 BB11+106	SET D31 = A32
	LDA 0 RUNKT+117	A24
L260	STA 0 BB11+105	SET D23 = A24
	STA 0 BB11+111	SET D41 = A42
	LDA 0 RUNKT+122	A33
	STA 0 BB11+107	SET D32 = A33
	LDA 0 RUNKT+125	A34
	STA 0 BB11+110	SET D33 = A34
	STA 0 BB11+112	SET D42 = A43
	LDA 0 RUNKT+130	A44
	STA 0 BB11+113	SET D43 = A44
	ENI 0 0	
	ENI 3 2	FOR USE 6TH WORD HENCE
	SLJ 4 MATRIX	MULT. B INVERSE BY D
	ZRO 0 L270-2	THIS WORD NOT USED
	ZRO 0 0	
	ZRO 0 0	
	ZRO 0 4	4 = CODE TO MATRIC MULTIPLY
L270	ZRO 0 4	L = 4 ROWS IN B INVERSE
	ZRO 0 BB11+120	BB11+120 = ADDRESS OF B INVERSE
	ZRO 0 4	N = 4 COLUMNS IN B INVERSE
	ZRO 0 BB11+100	BB11+100 = ADDRESS OF D MATRIX
	ZRO 0 3	M = 3 COLS. IN THE MATRIX PROD.

	ZRO	0	BB11+1	BB11+1 = ADDRESS OF MATRIX PROD.
	REM			L273-306 SETS UP MATRIX OF SYSTEM TO BE
	REM			SOLVED FOR DELTAUFIN, VAREL, VAREM AND VAREN
	LDA	3	BB11+12	
	STA	3	B42	
	IJP	3	/-1	
	ENI	3	2	
	LDA	3	BB11+7	
	STA	3	R32	
	IJP	3	/-1	
	ENI	3	2	
	LDA	3	BB11+4	
	STA	3	B22	
L300	IJP	3	/-1	
	LDA	0	RUNKT+11	UDOTFIN
	FSB	0	CAPUDFN	UDOTFIN - CAPUDFN (OR PASS IF REND. POINT FIXED
	STA	0	BB11	
	LDA	0	RUNKT+14	VDOTFIN
	FSB	0	CAPVDFN	VDOTFIN - CAPVDFN (OR PASS IF REND. POINT FIXED
	STA	0	B21	
	LDA	0	RUNKT+12	UFIN
	FSB	0	CAPUFIN	UFIN - CAPUFIN (OR PASS IF REND. POINT FIXED)
	STA	0	B31	
	LDA	0	RUNKT+15	VFIN
	FSB	0	CAPVFIN	VFIN - CAPVFIN (OR PASS IF REND. POINT FIXED)
	STA	0	B41	
	SLJ	0	L310	BYPASS PRINT OUT
	STA	0	BB11	PARAMETER WORD TO PRINT
L310	ZRO	0	C4	
	ENI	0	0	
	SLJ	4	MATRIX	INVERT SYSTEM MATRIX
	SLS	0	L310+1	SINGULAR MATRIX ALARM HALT
	ZRO	0	0	
	ZRO	0	0	
	ZRO	0	5	5 = CODE TO INVERT
	ZRO	0	4	L = 4
	ZRO	0	BB11	BB11 = ADDRESS OF MATRIX
	ZRO	0	0	N=0 NOT USED
	ZRO	0	0	
	ZRO	0	0	M=0 NOT USED
	ZRO	0	BB11+120	BB11+120 = ADDRESS OF INVERSE
	ENI	0	0	
	SLJ	4	MATRIX	MULT. INVERSE BY COL. MATRIX
	ZRO	0	L320-1	THIS WORD NOT USED
	ZRO	0	0	
L320	ZRO	0	0	
	ZRO	0	4	4 = CODE TO MATRIC MULTIPLY
	ZRO	0	4	L = 4 ROWS IN INVERSE
	ZRO	0	BB11+120	BB11+120 = ADDRESS OF INVERSE
	ZRO	0	4	N = 4 COLS. IN INVERSE
	ZRO	0	C1	C1 = ADDRESS OF COLUMN MATRIX
	ZRO	0	1	M=1 COL. IN THE COL. MATRIX
	ZRO	0	C1+4	C1+4= ADD. OF COL. MATRIX RESULT
	ENI	0	0	
	SLJ	0	/+2	BYPASS PRINT OUT
	STA	0	BB11	PARAMETER WORD TO PRINT
	ZRO	0	C1+7	
	ENI	0	0	
	ENI	0	0	
	ENI	0	0	
	ENI	0	0	
L330	ENI	0	0	
	ENI	0	0	
	ENI	0	0	
	ENI	0	0	
	IJP	6	/+1	JUMP IF B6 NOT = ZERO
	SLJ	0	FINAL	B6 = 0. JUMP TO FINAL PROG.
	SIU	6	/+1	
	SLS	2	/+1	STOP SWITCH
	ENI	6	0	RESET B6

	ENI	1	3	
	LDA	1	C1+4	
	STA	1	VARTAU	STORE DELTAUFIN,VAREL,VAREM,VAREN
	IJP	1	/-1	
	FAD	0	TAUFIN	NEW TAUFIN FOR NEXT ITERATE
	STA	0	SAVE+143	STORE NEW TAUFIN (NOTE L30+3)
L340	ENI	0	0	OR SLJ 0 L350+5 IF REND. POINT FIXED
	FMU	0	W	
	FAD	0	S	
	STA	0	SPWT	
	SLJ	4	TRIG+70	
	STA	0	COSSPWT	
	FMU	0	R	
	STA	0	SAVE+136	NEW CAPYFIN
	LDA	0	SPWT	
	SLJ	4	TRIG	
	ZRO	0	0	
	STA	0	SINSPWT	
	FMU	0	R	
	STA	0	SAVE+135	NEW CAPXFIN
	LDA	0	COSSPWT	
	FMU	0	V	
L350	STA	0	SAVE+137	NEW CAPUFIN
	LAC	0	SINSPWT	
	FMU	0	V	
	STA	0	SAVE+140	NEW CAPVFIN
	LAC	0	COSSPWT	
	FMU	0	VSQDR	
	STA	0	SAVE+142	NEW CAPVDFN
	LAC	0	SINSPWT	
	FMU	0	VSQDR	
	STA	0	SAVE+141	NEW CAPUDFN
	ENI	0	0	
	ENI	0	0	
	ENI	1	2	
	LDA	1	C1+5	
	FAD	1	EL	
	STA	1	EL	STORE NEW EL, EM AND EN
L360	IJP	1	/-1	
	SLJ	4	70007	PRINT
	ZRO	0	0	
	SAU	0	MDOT	DECIMAL DUMP WITH PANEL
	ZRO	0	S	
	EXF	0	70	CLEAR ARITH. ERRORS
	SLJ	4	70007	PRINT
	STA	0	CAPXFIN	DEC. DUMP
	ZRO	0	LAM	
	SLJ	0	RECUR	TO NEXT ITERATION
	ZRO	0	0	
	BSS		3	
POLAR	BSS		200	B1=33 B6=66370 P=460
EL1	BSS		1	
EM1	BSS		1	
EN1	BSS		1	
T1	BSS		1	
EL2	BSS		1	
EM2	BSS		1	
EN2	BSS		1	
T2	BSS		1	
EL3	BSS		1	
EM3	BSS		1	
EN3	BSS		1	
T3	BSS		1	
EL4	BSS		1	
EM4	BSS		1	
EN4	BSS		1	
T4	BSS		1	
EL5	BSS		1	
EM5	BSS		1	
EN5	BSS		1	

T5	BSS	1	
	BSS	26	STORE FOR MATRIX PRODUCT
FINAL	ENI	1 147	COMPUTES POINTS ON FINAL TRAJ.
	LIL	2 FIXIPLON	
	LDA	1 SAVE	
	STA	1 RUNKT	RESET INITIAL CONDITIONS
	IJP	1 /-1	
	SLJ	4 ALPHA	SET UP GILL ROUTINE
	ZRO	0 RUNKT	PARAMETER WORD
	ZRO	0 DERIV	
	ENI	0 0	
	SLJ	4 /+4	RET.JUMP TO DUMP SUBROUTINE
	IJP	2 /+1	JUMP IF B2 NOT = ZERO
L650	SLJ	0 L700+1	B2=0. JUMP TO REMAINDER OF FINAL PROG.
	ENI	0 0	
	SLJ	4 ALPHA+1	INTEGRATE AGAIN
	ENI	0 0	
	SLJ	0 /-3	
	SLJ	0 0	ENTRY TO DUMP SUBROUTINE
	LDA	0 RUNKT+2	TAU
	ENI	0 0	
	ENI	0 0	
	STA	0 DUMP	(DUMP) = TAU
	LDA	0 RUNKT+4	X
	ENI	0 0	
	ENI	0 0	
	STA	0 DUMP+4	(DUMP+4) = X
	LDA	0 RUNKT+7	Y
	ENI	0 0	
L660	ENI	0 0	
	STA	0 DUMP+5	(DUMP+5) = Y
	LDA	0 RUNKT+12	U
	ENI	0 0	
	ENI	0 0	
	STA	0 DUMP+6	(DUMP+6) = U
	LDA	0 RUNKT+15	V
	ENI	0 0	
	ENI	0 0	
	STA	0 DUMP+7	(DUMP+7) = V
	LDA	0 RUNKT+11	UDOT
	ENI	0 0	
	ENI	0 0	
	STA	0 DUMP+10	(DUMP+10) = UDOT
	LDA	0 RUNKT+14	VDOT
	ENI	0 0	
L670	ENI	0 0	
	STA	0 DUMP+11	(DUMP+11) = VDOT
	LDA	0 RUNKT+12	U
	LDQ	0 RUNKT+15	V
	SLJ	4 POLAR+130	
	ENI	0 0	
	ENI	0 0	
	STQ	0 DUMP+12	(DUMP+12) = ARCTAN(V/U)
	LDA	0 LAM	
	LDQ	0 MU	
	SLJ	4 POLAR+130	
	ENI	0 0	
	ENI	0 0	
	STQ	0 DUMP+13	(DUMP+13) = ARCTAN(MU/LAM)
	SLJ	4 70007	PRINT
	STA	0 DUMP	PARAMETER WORD
	ZRO	0 DUMP+13	
L700	SLJ	0 L650+2	TO EXIT OF DUMP S.R.
	ZRO	0 0	
	LDA	0 C3	C3 = CAPXFIN - XFIN
	ENI	0 0	
	ENI	0 0	
	STA	0 DUMP+14	(DUMP+14) = CAPXFIN - XFIN
	LDA	0 C4	C4 = CAPYFIN - YFIN
	ENI	0 0	

	ENI	0	0	
	STA	0	DUMP+15	(DUMP+15) = CAPYFIN - YFIN
	LDA	0	C1	C1 = CAPUFIN - UFIN
	ENI	0	0	
	ENI	0	0	
	STA	0	DUMP+16	(DUMP+16) = CAPUFIN - UFIN
	LDA	0	C2	C2 = CAPVFIN - VFIN
	ENI	0	0	
L710	ENI	0	0	
	STA	0	DUMP+17	(DUMP+17) = CAPVFIN - VFIN
	SLJ	4	70007	PRINT
	ZRO	0	0	
	STA	0	DUMP+14	PARAMETER WORD
	ZRO	0	DUMP+17	
	SLJ	0	L3570+5	JUMP TO PRINT B FINAL
	ZRO	0	0	
STOR1	BSS	1		
STOR2	BSS	1		
STOR3	BSS	1		
STOR4	BSS	1		
L720	DEC	1.		
DELX1	BSS	1		
DELY1	BSS	1		
DELU1	BSS	1		
DELV1	BSS	1		
	DEC	1.		
DELX2	BSS	1		
DELY2	BSS	1		
DELU2	BSS	1		
DELV2	BSS	1		
	DEC	1.		
DELX3	BSS	1		
DELY3	BSS	1		
DELU3	BSS	1		
DELV3	BSS	1		
	DEC	1.		
DELX4	BSS	1		
DELY4	BSS	1		
DELU4	BSS	1		
DELV4	BSS	1		
	DEC	1.		
DELX5	BSS	1		
DELY5	BSS	1		
DELU5	BSS	1		
SAVE	BSS	150		ALSO DELV5 STORE
RUNKT	BSS	135		
CAPXFIN	BSS	1		
CAPYFIN	BSS	1		
CAPUFIN	BSS	1		
CAPVFIN	BSS	1		
CAPUDFN	BSS	1		
CAPVDFN	BSS	1		
TAUFIN	BSS	1		
LAM	BSS	1		
HYP	BSS	1		
HYP3	BSS	1		
MU	BSS	1		
HYP2	BSS	1		
UNITY	DEC	1.		
W	BSS	1		
DELTAU	BSS	1		
SPWT	BSS	1		
COSSPWT	BSS	1		
SINSPWT	BSS	1		
R32	BSS	1		
R52	BSS	1		
INTSIGN	BSS	1		
FRACSIGN	BSS	1		
FLOIPLON	BSS	1		
FIXIPLON	BSS	1		

THREDR2	OCT	2002417416663160	THREE/ROOT2
TREHALF	DEC	1.5	
DELTFLSG	BSS	1	
NT	BSS	1	
THETA	BSS	1	
VSTART	DEC	.65	NON-DIMEN. INITIAL SPEED
DELTHETA	BSS	1	
DELXFIN	BSS	1	
DELYFIN	BSS	1	
DELUFIN	BSS	1	
DELVFIN	BSS	1	
MDOT	DEC	.0025	FRACTIONAL MASS LOSS PER SEC.
A	BSS	1	
QQ	BSS	1	
C	DEC	10000.	ROCKET NOZZLE VEL. IN FT./SEC.
EL	BSS	1	
EM	BSS	1	
EN	BSS	1	
S	BSS	1	INIT. TARGET SECTOR ANGLE
A1	BSS	1	
A2	BSS	1	
A3	BSS	1	
A4	BSS	1	
VARTAU	BSS	1	
VAREL	BSS	1	
VAREM	BSS	1	
VAREN	BSS	1	
ALPHA	BSS	134	B1=30 B6=67340 P=460
	BSS	14	
DUMP	BSS	20	
BB11	BSS	1	
B12	BSS	1	
B13	BSS	1	
B14	BSS	1	
B21	BSS	1	
B22	BSS	1	
B23	BSS	1	
B24	BSS	1	
B31	BSS	1	
B32	BSS	1	
B33	BSS	1	
B34	BSS	1	
B41	BSS	1	
B42	BSS	1	
B43	BSS	1	
B44	BSS	1	
	BSS	120	5 TIMES L SQUARED CELLS
C1	BSS	1	
C2	BSS	1	
C3	BSS	1	
C4	BSS	1	
	BSS	4	STORE FOR MATRIX PRODUCT
LOG	BSS	100	B1=12 B6=67700 P=460
	REM		LOG S.R. ALARM EXIT TO K110
	REM		(67703) = 750 65110 000 00000
L2000	BSS	1440	USNPGS GEN. DUMP B1=32 P=21
	REM		AID TO LINEARIZED TRAJECTORY PROG.
L3440	ENA	0 0	
	ENI	1 17	
	STA	1 BB11	CLEAR BB11 MATRIX AREA
	IJP	1 /	
	LDA	0 TAUFIN	
	SLJ	4 TRIG	
	STA	0 BB11	(BB11) = SINT.
	LDA	0 TAUFIN	
	SLJ	4 TRIG+70	
	ZRO	0 0	
	STA	0 B21	(B21) = COST
	LDA	0 TAUFIN	
	FMU	0 ROOT2	

	SLJ 4 EXP+71	
	STA 0 B32	(B32) = SINHTR2
L3450	LDA 0 TAUFIN	
	FMU 0 ROOT2	
	SLJ 4 EXP+107	
	STA 0 B42	(B42) = COSHTR2
	LDA 0 SIN	SINE IMPULSE INTEGRAL
	FDV 0 C	
	STA 0 B13	
	LDA 0 COS	COSINE IMPULSE INTEGRAL
	FDV 0 C	
	STA 0 B23	
	LDA 0 SINH	SINH IMPULSE INTEGRAL
	FDV 0 C	
	STA 0 B33	
	LDA 0 COSH	COSH IMPULSE INTEGRAL
	FDV 0 C	
	STA 0 B43	
L3460	LAC 0 CAPYFIN	
	STA 0 B14	
	LAC 0 CAPVFIN	
	STA 0 B24	
	SLJ 0 L3570+3	JUNMP TC PATCH
	STA 0 B34	
	LDA 0 CAPUFIN	
	STA 0 B44	
	LAC 0 DELXFIN	
	STA 0 C1	C1 = ADD. OF MATRIX COL.
	LAC 0 DELUFIN	
	STA 0 C2	
	LAC 0 DELYFIN	
	FMU 0 ROOT2	
	STA 0 C3	
	LAC 0 DELVFIN	
	STA 0 C4	
L3470	ENA 0 /+2	
	SAL 0 L320+4	CREATE LINEAR EQU. ROUTINE EXIT
	SLJ 0 L310	JUMP TO LINEAR EQU. ROUTINE
	ZRO 0 0	
	ENA 0 L320+6	
	SAL 0 L320+4	REBUILD RENDEVOUS PROGRAM
	LDA 0 C1+4	DEL V1
	FAD 0 V1	(STOR1) = NEW V1
	STA 0 STOR1	
	FMU 0 STOR1	(STOR2) = NEW V1 SQUARED
	STA 0 STOR2	DEL V2
	LDA 0 C2+4	
	FAD 0 V2	(STOR3) = NEW V2
	STA 0 STOR3	
	FMU 0 STOR3	NEW V1 SQ. + NEW V2 SQ.
	FAD 0 STOR2	
L3500	SLJ 4 SQR00T	
	ZRO 0 0	NEW VSTART
	STA 0 VSTART1	NEW V1
	LDA 0 STOR1	COSINE NEW THETA
	FDV 0 VSTART1	TO INVERSE COSINE S.R.
	SLJ 4 POLAR	NEW THETA
	STA 0 THETA1	DEL C
	LDA 0 C3+4	NEW C
	FAD 0 C	(EJECT) = NEW C
	STA 0 EJECT	DIFFERENTIAL OF B
	LDA 0 C4+4	NEW B
	FAD 0 B	(SECTOR) = NEW B
	STA 0 SECTOR	PRINT RESULTS DECIMAL
	SLJ 4 70007	PARAMETER WORD
	STA 0 VSTART1	
	ZRO 0 SECTOR	PRINT RESULTS OCTAL
L3510	SLJ 4 70007	
	ZRO 0 0	PARAMETER WORD
	ZRO 0 VSTART1	

	ZRO	0	SECTOR	
	ENI	0	0	
	ENI	0	0	
	LDA	0	VSTART1	RESUME COMP. OF INIT. CONDITIONS
	STA	0	VSTART	SET NEW VSTART
	LDA	0	THETA1	
	STA	0	THETA	SET NEW THETA
	LDA	0	EJECT	
	STA	0	C	SET NEW C
	LDA	0	SECTOR	
	STA	0	B	SET NEW B
	SLJ	4	TRIG+70	
L3520	ZRO	0	0	
	STA	0	COSB	
	FMU	0	R	
	STA	0	CAPYFIN	TARGET COOR. AT RENDEVOUS
	LDA	0	B	
	SLJ	4	TRIG	
	ZRO	0	0	
	STA	0	SINB	
	FMU	0	R	
	STA	0	CAPXFIN	TARGET COOR. AT RENDEVOUS
	LDA	0	COSB	
	FMU	0	V	
	STA	0	CAPUFIN	TARGET VEL. COMP. AT RENDEVOUS
	LAC	0	SINB	
	FMU	0	V	
	STA	0	CAPVFIN	TARGET VEL. COMP. AT RENDEVOUS
L3530	LAC	0	COSB	
	FMU	0	VSQDR	
	STA	0	CAPVDFN	TARGET ACC. COMP. AT RENDEVOUS
	LAC	0	SINB	
	FMU	0	VSQDR	
	STA	0	CAPUDFN	TARGET ACC. COMP. AT RENDEVOUS
	LDA	0	THETA	
	SLJ	4	TRIG+70	COSINE THETA
	ZRO	0	0	
	FMU	0	VSTART	
	STA	0	V1	INITIAL HORIZONTAL VEL.
	LDA	0	THETA	
	SLJ	4	TRIG	SINE THETA
	FMU	0	VSTART	
	STA	0	V2	INITIAL VERTICAL VEL.
	LDA	0	C	ROCKET NOZZLE VEL.
L3540	FSB	0	TENGRAND	NOZZLE VEL. DIFFERENCE
	AJP	2	/+1	JUMP IF DIFF. IS POS.
	SCM	0	MASK	ABSO. VALUE OF DIFF.
	THS	0	UNITY	EXIT IF ONE GREATER THAN DIFF.
	SLJ	0	SECTOR+2	NO. JUMP TO ADJUST MDOT AND C
	LDA	0	C	YES. LOAD ROCKET NOZZLE VEL.
	FMU	0	MDOT	
	FDV	0	GACCEL	
	STA	0	A	NON-DIMEN. ACCELERATION
	LDQ	0	ELS	
	SLJ	0	K100+2	RETURN TO LIN. TRAJ. PROG.
VSTART1	BSS	1		TEMP. STORE FOR NEW VSTART
THETA1	BSS	1		TEMP. STORE FOR NEW THETA
EJECT	BSS	1		TEMP. STORE FOR NEW C
SECTOR	BSS	1		TEMP. STORE FOR NEW B
	SLS	0	SECTOR+1	HALT IF 1-WT IS NEGATIVE
	ZRO	0	0	
	LAC	0	TAUFIN	(-T)
	FMU	0	OMEGA	(-WT)
	FAD	0	UNITY	(1-WT)
	AJP	3	SECTOR+1	HALT IF 1-WT IS NEGATIVE
	SLJ	4	LOG+66	LOG(1-WT) TO BASE E
	ZRO	0	0	
	FMU	0	C	
	FDV	0	TENGRAND	
	SLJ	4	EXP	

L3560

ZRO 0 0
 SCM 0 MASK
 FAD 0 UNITY
 FDV 0 TAUFIN
 STA 0 OMEGA
 LDA 0 GACCEL
 FDV 0 REARTH
 SLJ 4 SQR00T
 ZRO 0 0
 FMU 0 OMEGA
 STA 0 MDOT
 LDA 0 TENGRAND
 STA 0 C
 ENI 0 0
 ENI 0 0
 ENI 0 0
 ENI 0 0
 ENI 0 0
 ENI 0 0
 ENI 0 0
 ENI 0 0
 LDA 0 MDOT
 FMU 0 C
 FDV 0 GACCEL
 STA 0 A
 SLJ 0 K70
 LDA 0 CAPXFIN
 FMU 0 RCOT2
 SLJ 0 L3460+2
 ZRO 0 0
 SLJ 4 70007
 ZRO 0 0
 STA 0 UNITY
 ZRO 0 SPWT
 SLS 0 L3570+7
 ZRO 0 0
 END

NEW OMEGA
 STORE NEW OMEGA

SHULER ANGULAR FREQ.

NEW MDOT
 STORE NEW MDOT
 LOAD NEW C
 STORE NEW C

L3570

STORE NEW A
 JUMP TO LIN. TRAJ. PROG.
 PATCH FCR L3460+1 L.I.

ENTRY FROM L710+3
 PRINT B FINAL DECIMAL
 PARAMETER WORD
 FINAL B = SPWT
 END OF NON-LINEAR PROGRAM

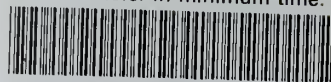
TA7 58303
.U6 Bleick
no.34 Orbital transfer in
minimum time.

10 SEP 71	20592
16 DEC 86	30573
23 MAY 87	31957

TA7 58303
.U6 Bleick
no.34 Orbital transfer in
minimum time.

genTA 7.U6 no.34

Orbital transfer in minimum time.



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